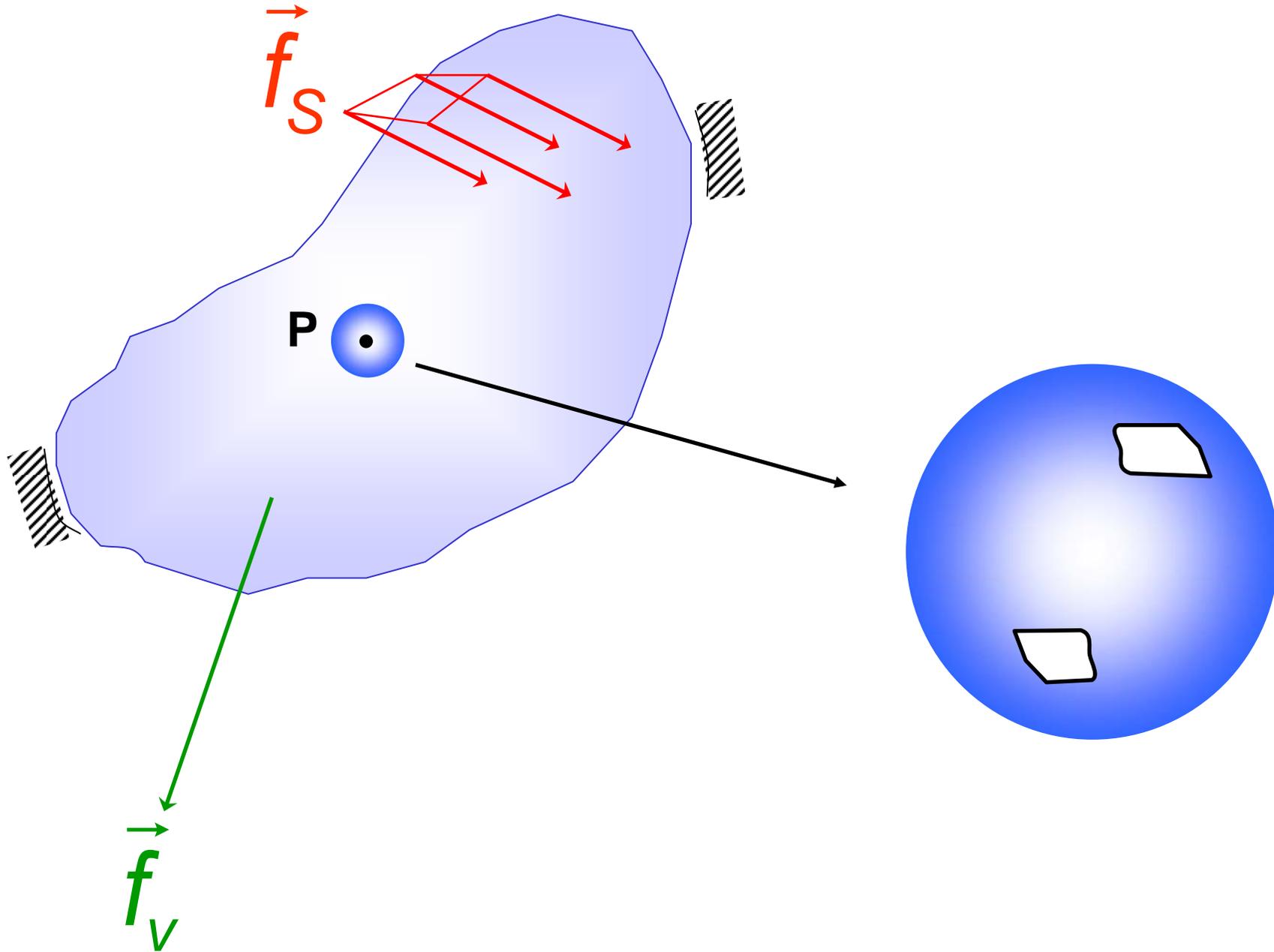
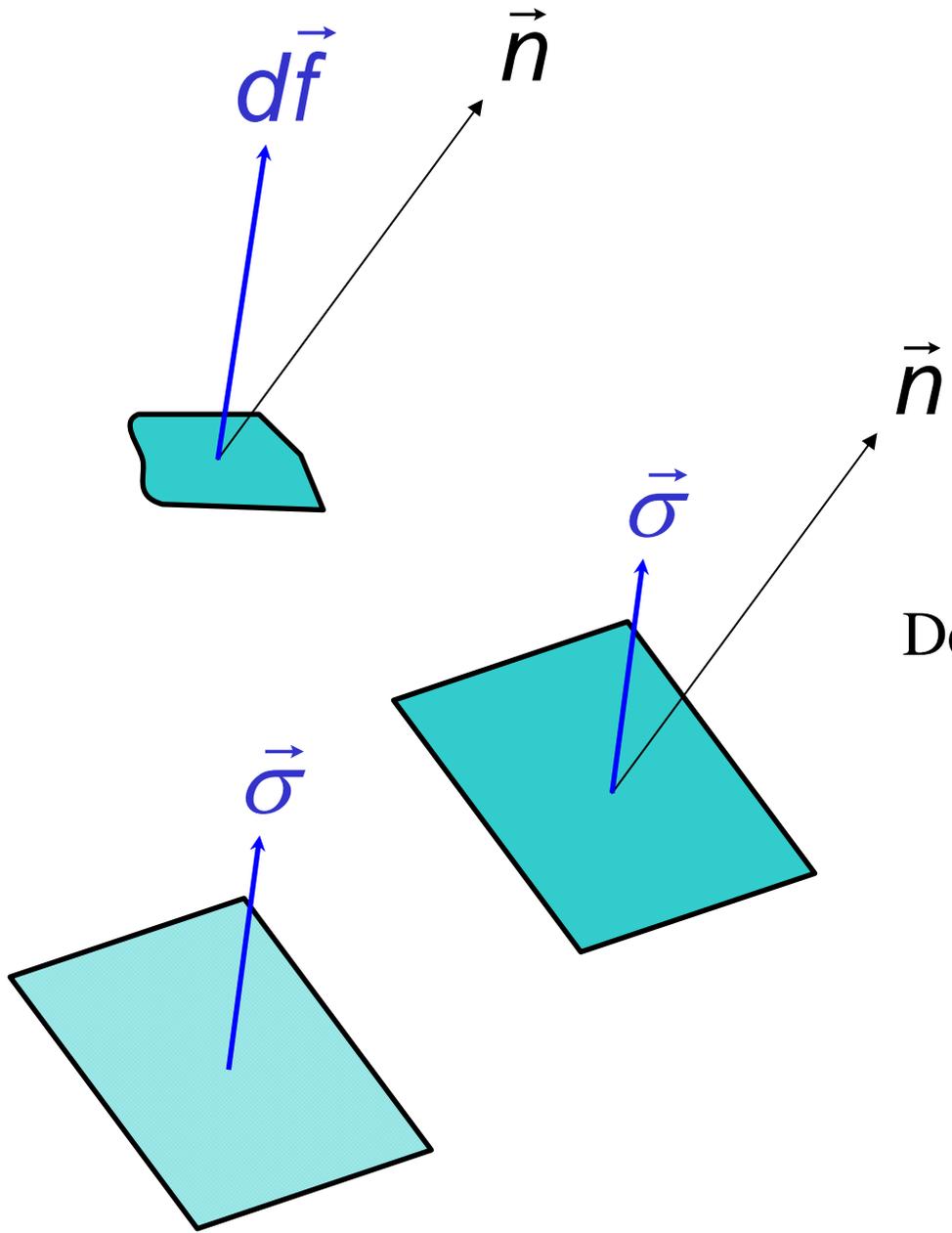


VECTOR TENSION



VECTOR TENSION

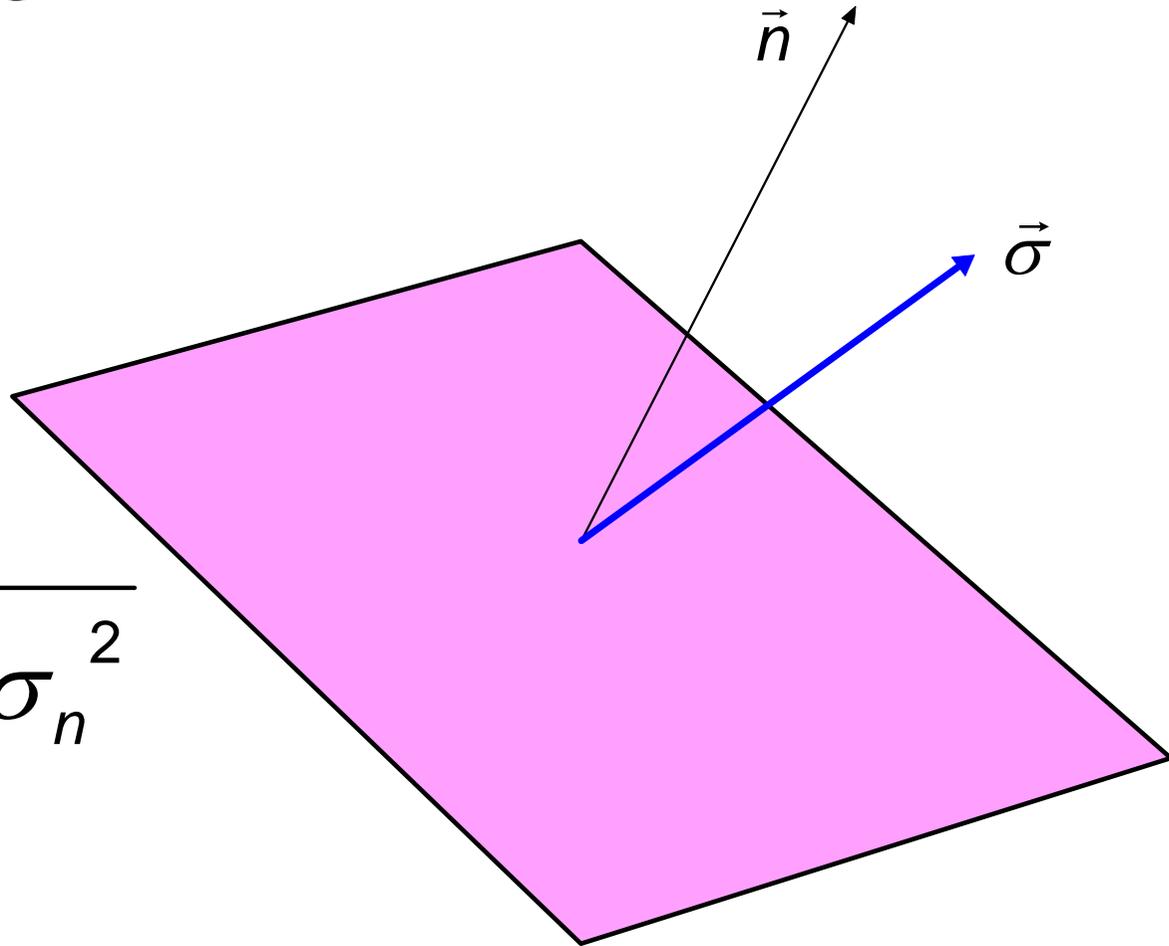


Depende de:

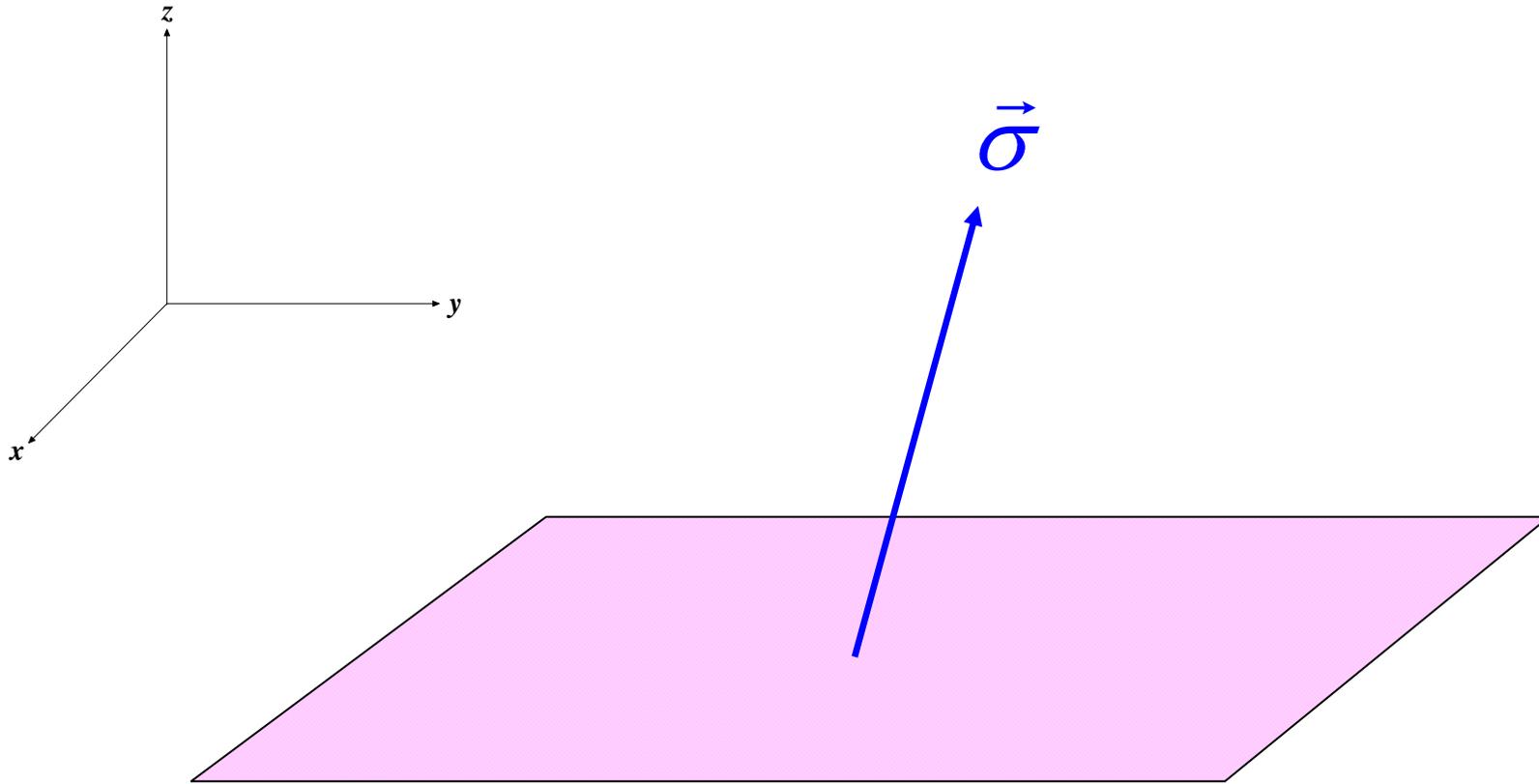
COMPONENTES INTRINSECAS

$$\sigma_n = \vec{n}^t \cdot \vec{\sigma}$$

$$\tau = \sqrt{|\vec{\sigma}|^2 - \sigma_n^2}$$



VECTOR TENSIÓN PARA LOS PLANOS COORDENADOS



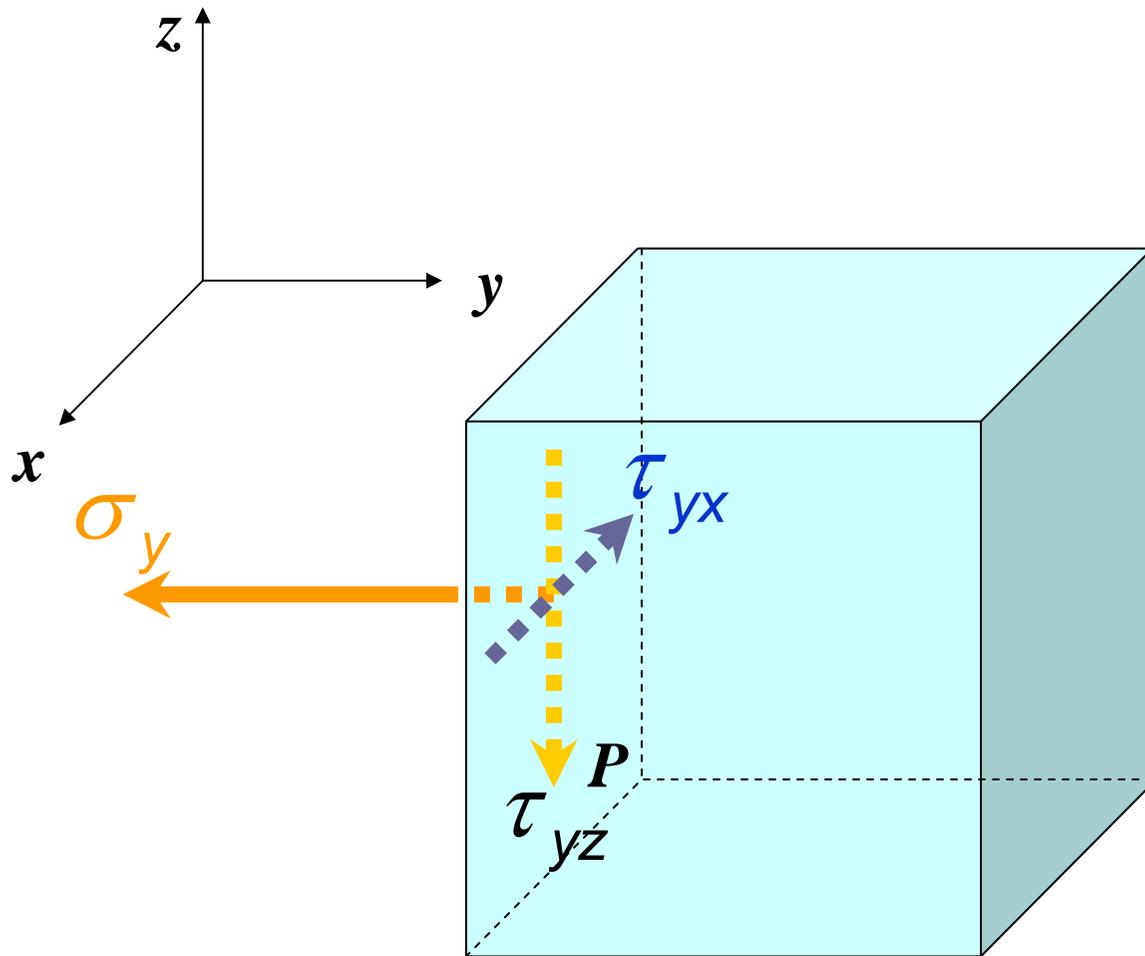
MATRIZ DE TENSIONES

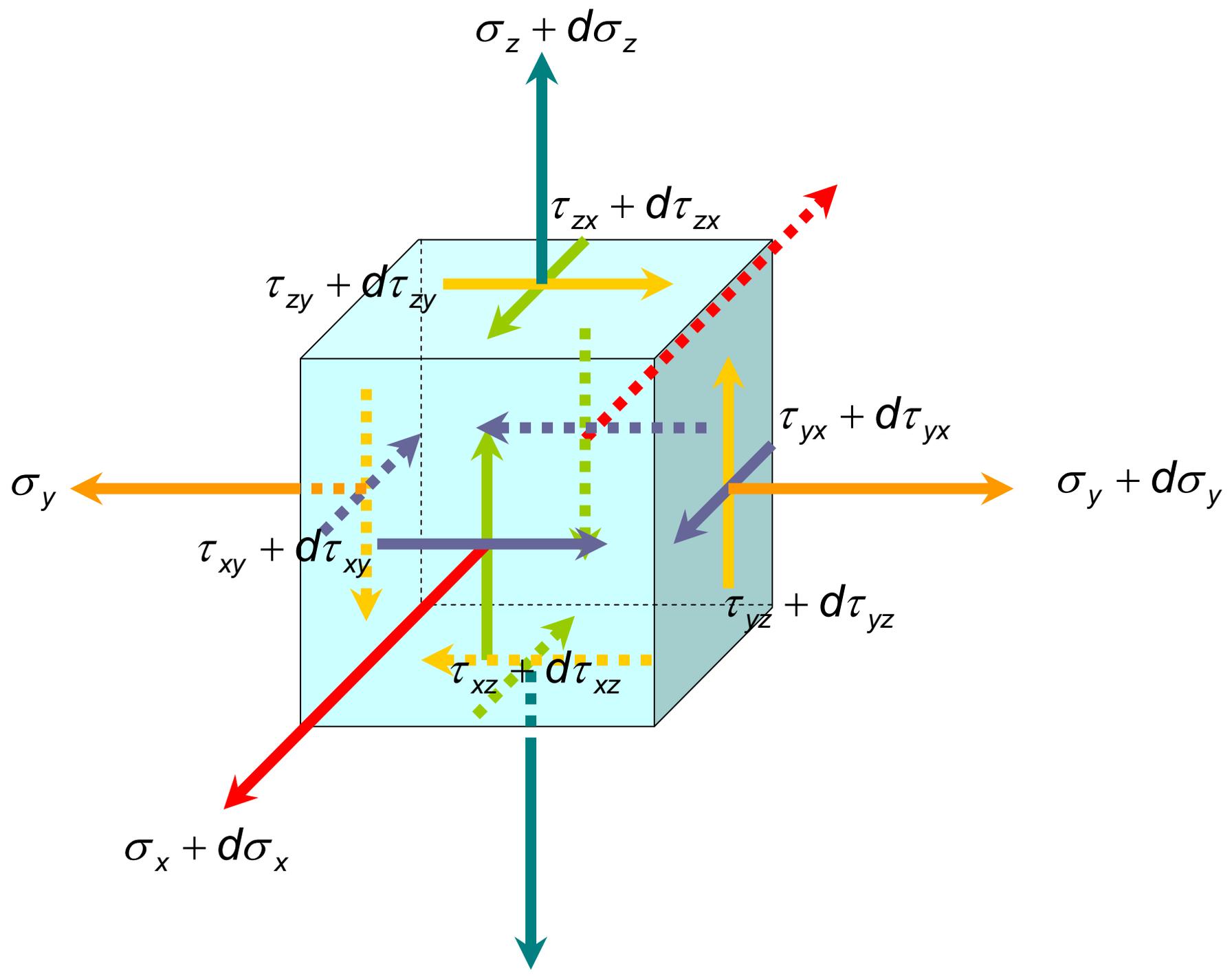
$$[T] = \begin{pmatrix} \sigma_x & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & \sigma_y & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & \sigma_z \end{pmatrix}$$

CARACTERÍSTICAS DE LA MATRIZ DE TENSIONES

- Relacionada con las fuerzas exteriores
- Sus componentes deben variar de forma

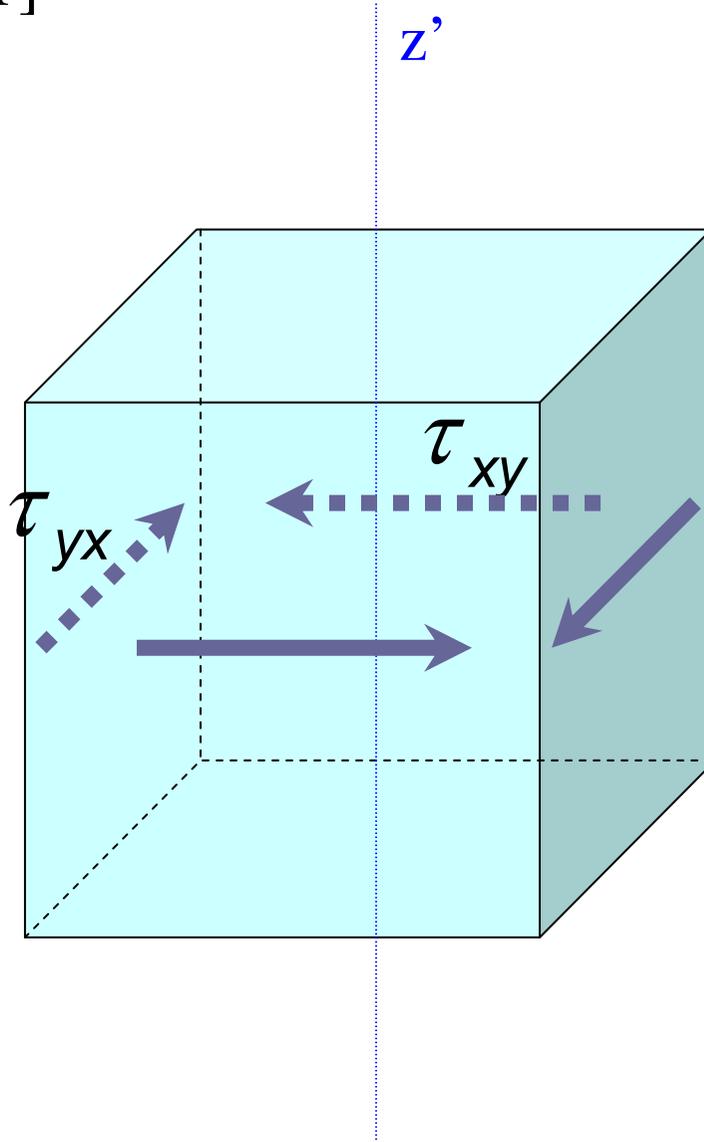
VARIACIÓN DE [T]:

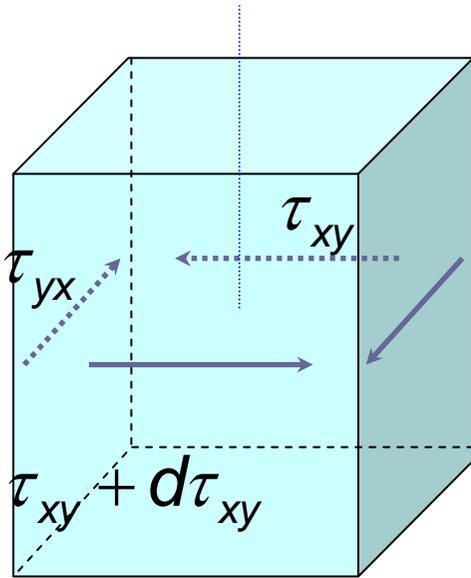




EQUILIBRIO ROTACIONAL
EN UN CUBO DIFERENCIAL:
SIMETRÍA DE [T]

$$\sum M_{z'} = 0$$





$$\tau_{yx} + d\tau_{yx}$$

$$\sum M_z = 0$$

$$\tau_{xy} dydz \frac{dx}{2} + (\tau_{xy} + d\tau_{xy}) dydz \frac{dx}{2} -$$

$$- \tau_{yx} dx dz \frac{dy}{2} - (\tau_{yx} + d\tau_{yx}) dx dz \frac{dy}{2} = 0$$

Hay otras dos
ecuaciones de
equilibrio:

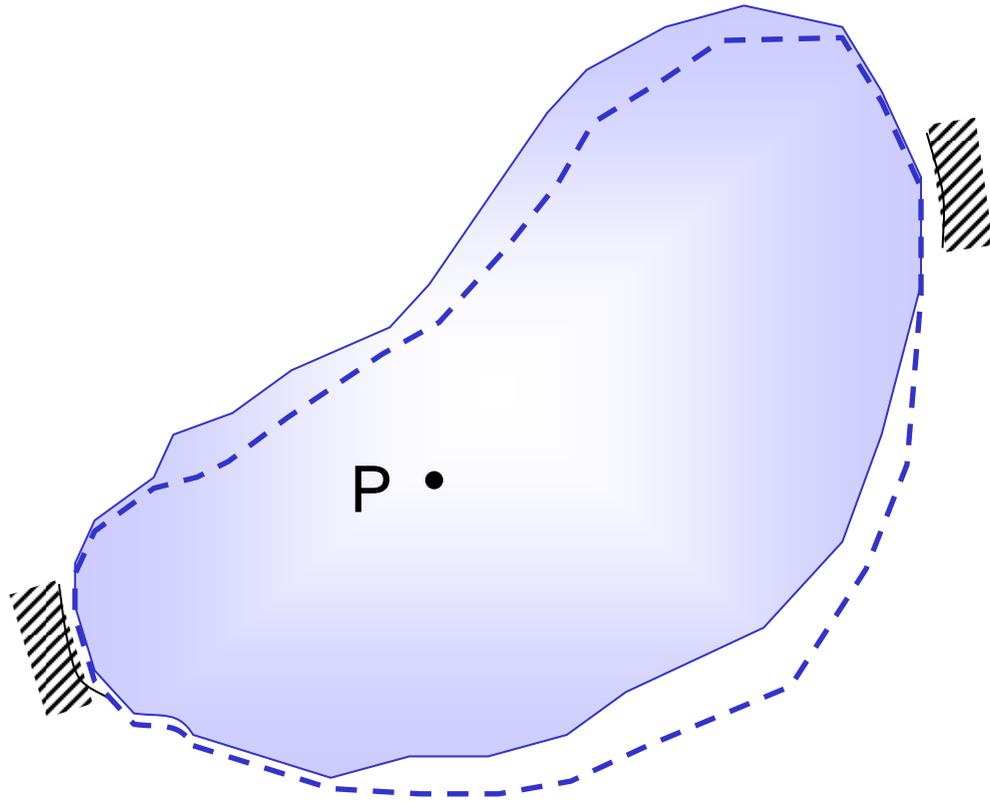
$$\sum M_y = 0 \rightarrow$$

$$\tau_{xz} = \tau_{zx}$$

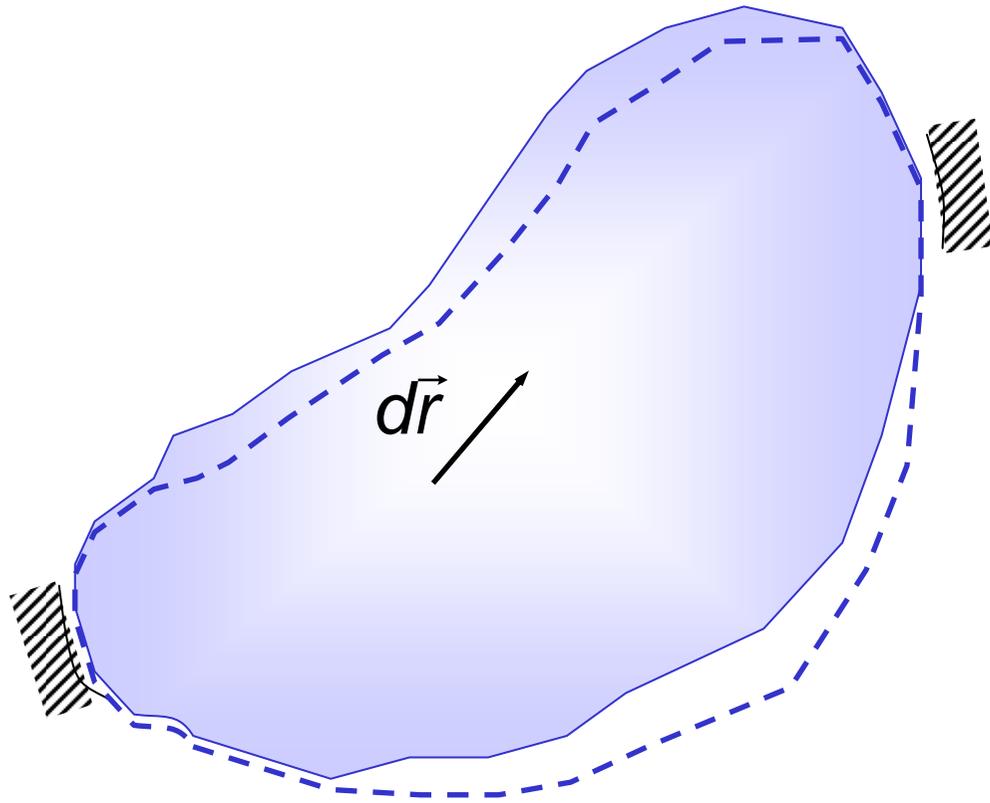
$$\sum M_x = 0 \rightarrow$$

$$\tau_{yz} = \tau_{zy}$$

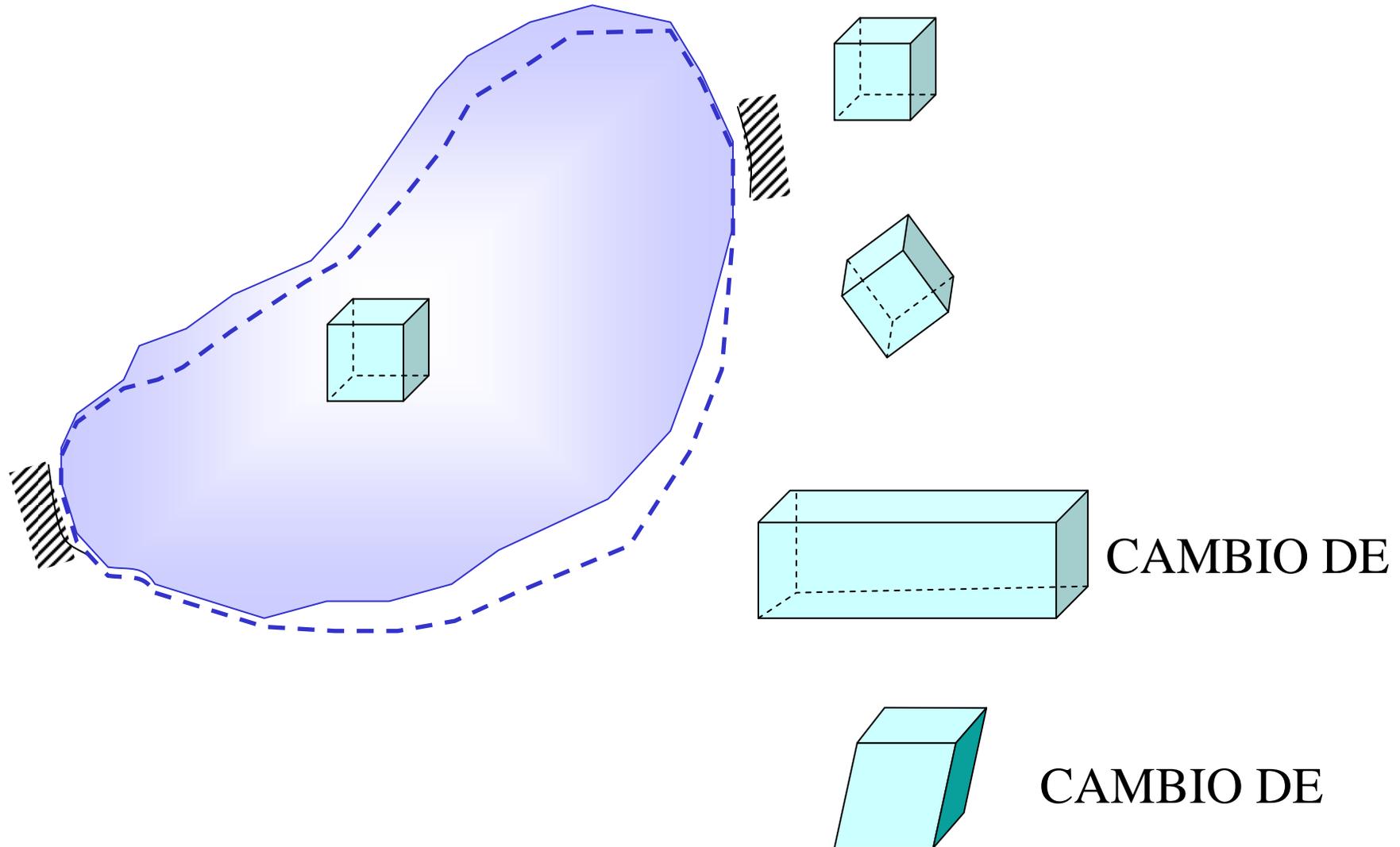
DEFORMACIÓN



DEFORMACIÓN

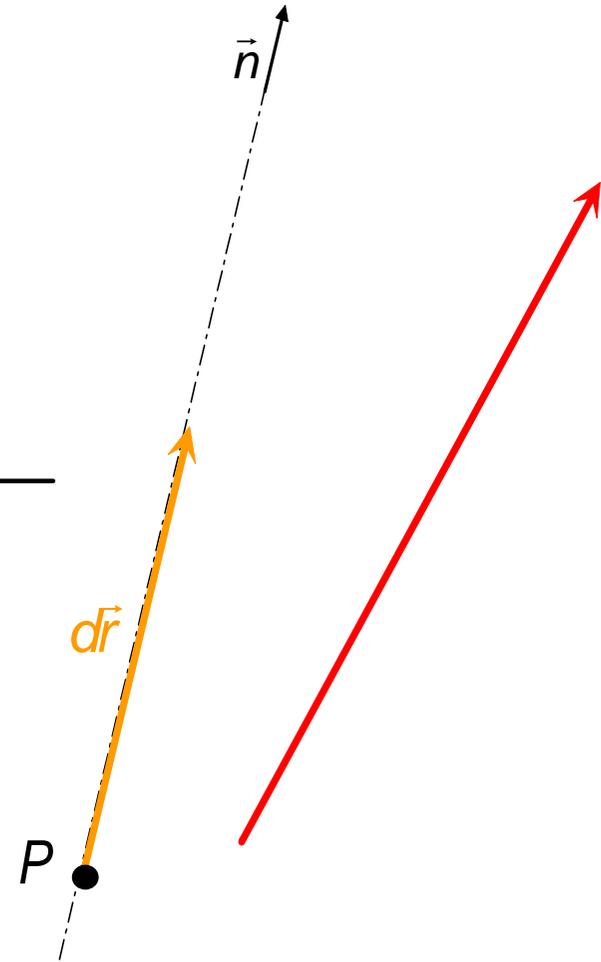


DEFORMACIÓN

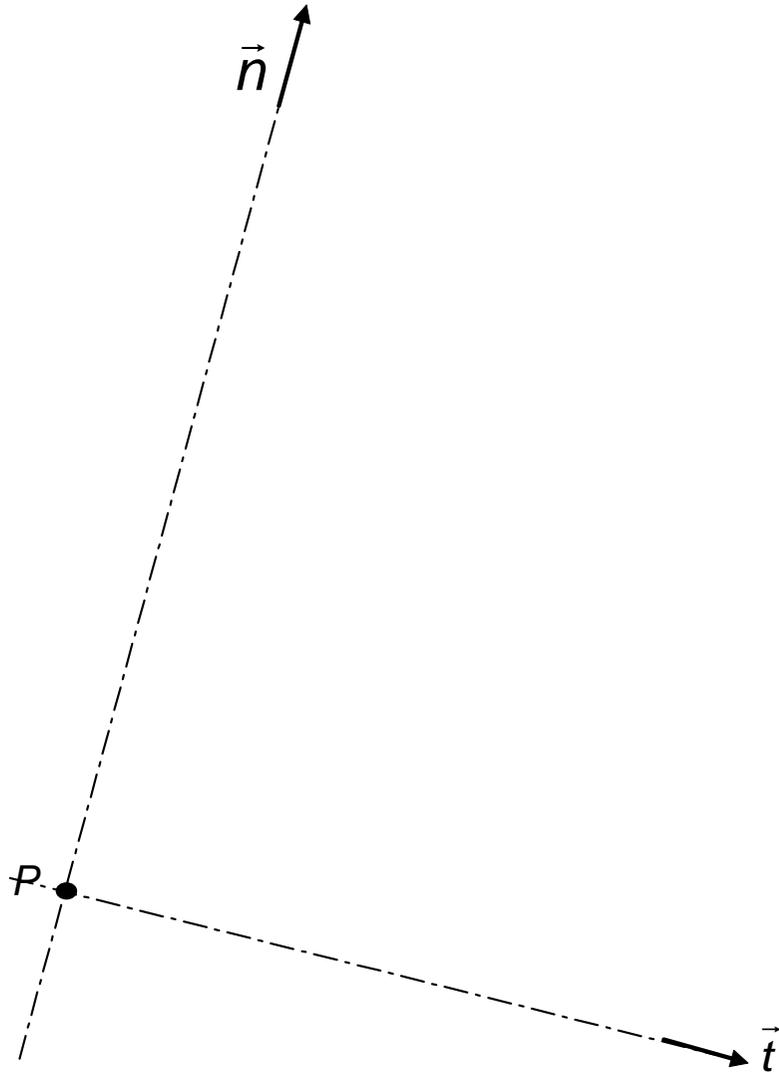


Deformación longitudinal (unitaria)

$$\epsilon_n = \text{-----} = \text{-----}$$



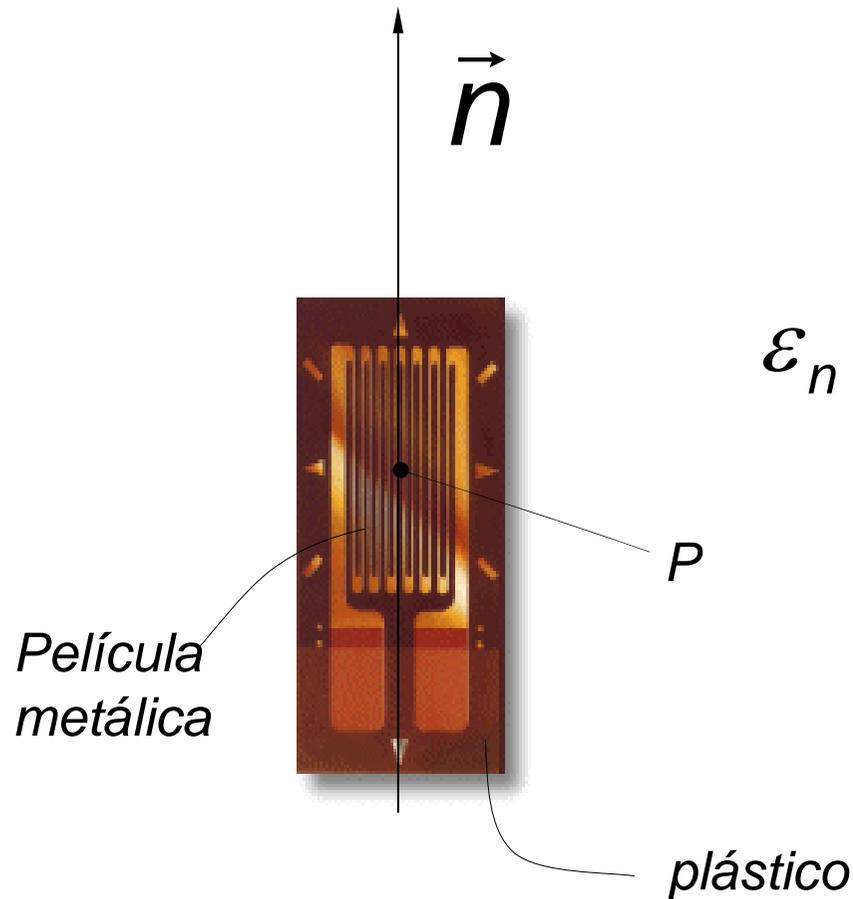
Deformación angular γ_{nt}



$$\gamma_{nt} =$$

Sensores de deformación: Galga extensométrica (strain gage/gauge)

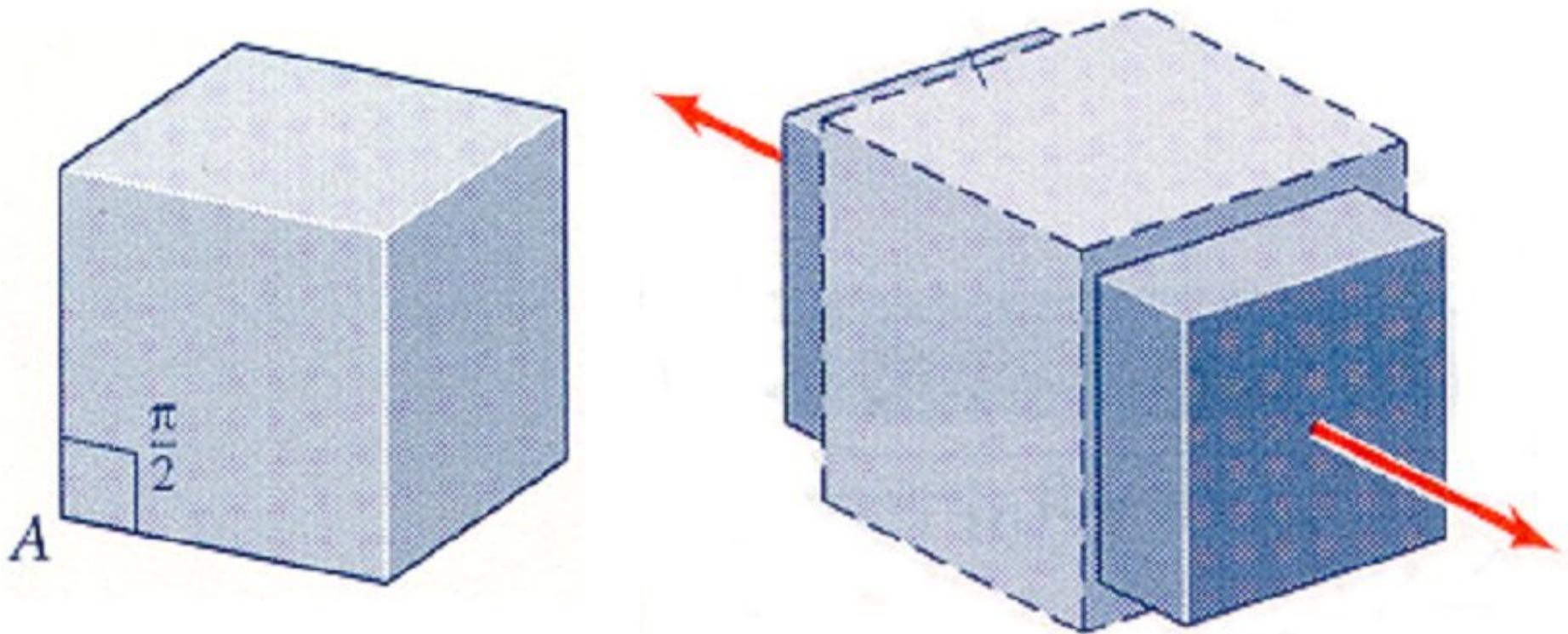
$$\varepsilon_n = \varepsilon_x \alpha^2 + \varepsilon_y \beta^2 + \varepsilon_z \gamma^2 + \gamma_{xy} \alpha \beta + \gamma_{xz} \alpha \gamma + \gamma_{yz} \beta \gamma$$

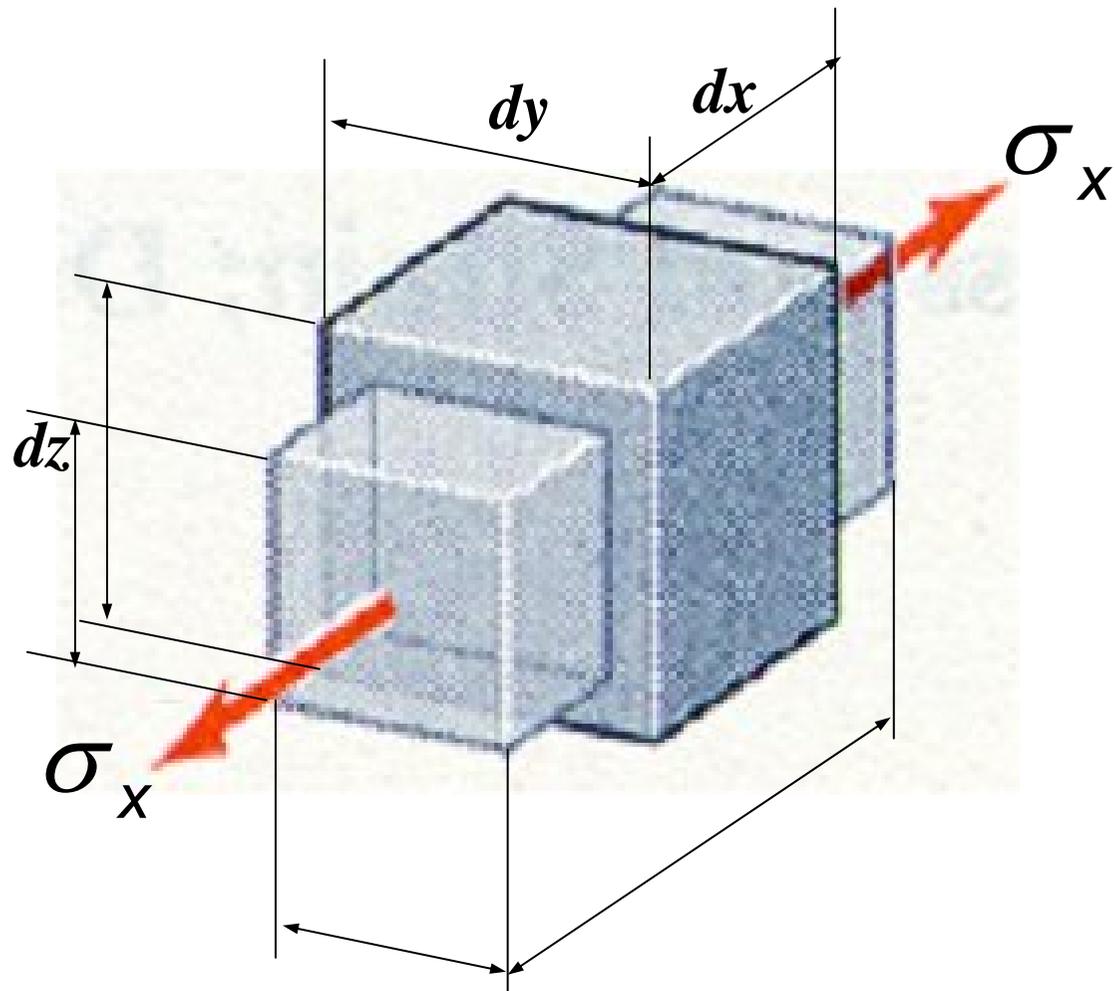


$$\varepsilon_n = \frac{\Delta dL}{dL} \cong \frac{\Delta R}{R} = K \frac{\Delta R}{R}$$

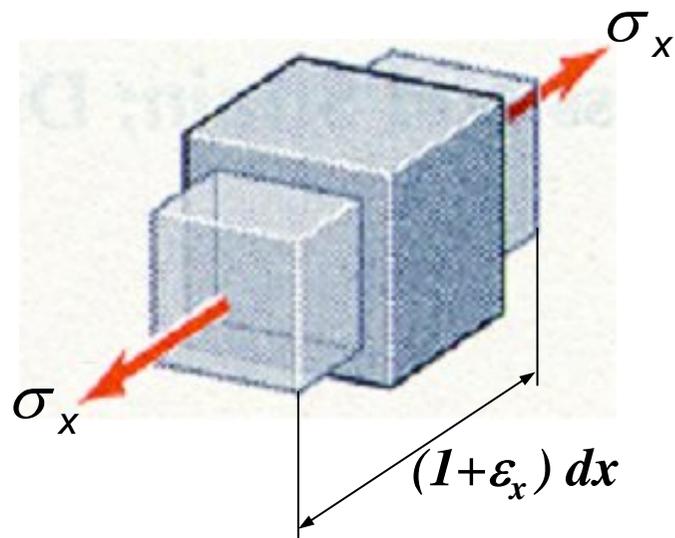
RELACIONES TENSIÓN-DEFORMACIÓN

Sólido elástico:



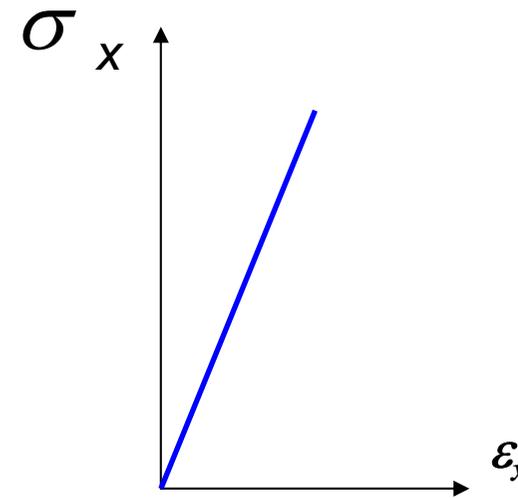


Sólido elástico lineal: Relación lineal entre tensiones y deformaciones



$$\sigma_x = E \cdot \varepsilon_x$$

E: Módulo de elasticidad



- E siempre

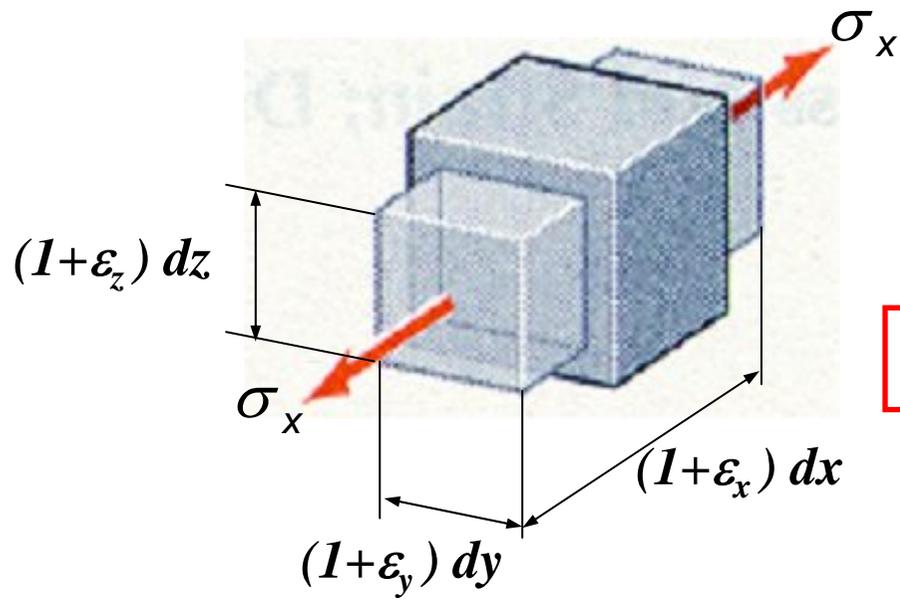
- [E]: Unidades de

-Valores:

Aceros no inoxidable: $E = 2,1 \cdot 10^5 \text{ MPa} = 2 \cdot 10^6 \text{ kp/cm}^2$

Aluminios: $E = 0,7 \cdot 10^5 \text{ MPa}$

Polímeros: $E \approx 10^3 \text{ MPa}$



$$\varepsilon_y = \varepsilon_z = -\nu \cdot \varepsilon_x = -\frac{\nu}{E} \sigma_x$$

ν : Coeficiente de

- ν casi siempre

- $[\nu]$:

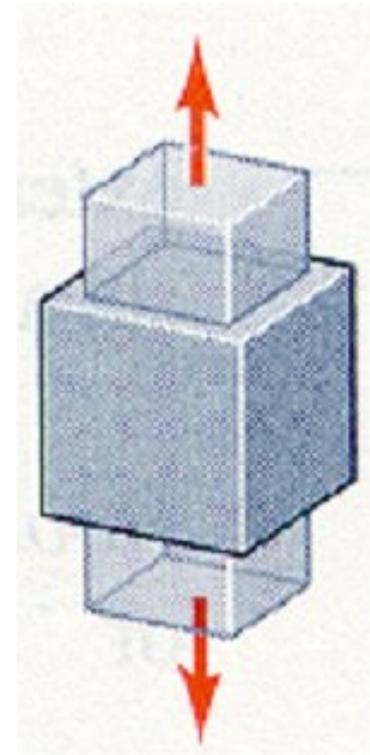
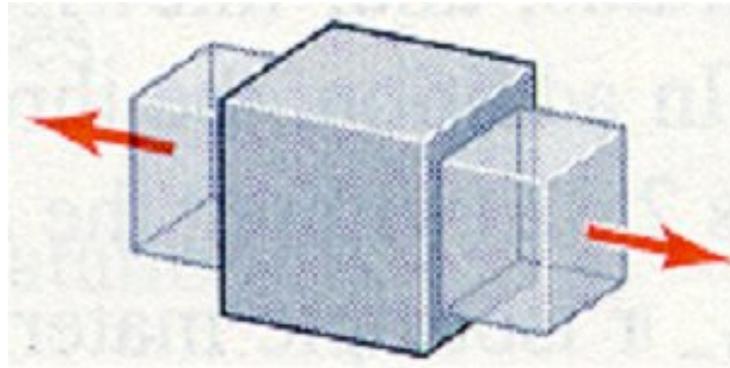
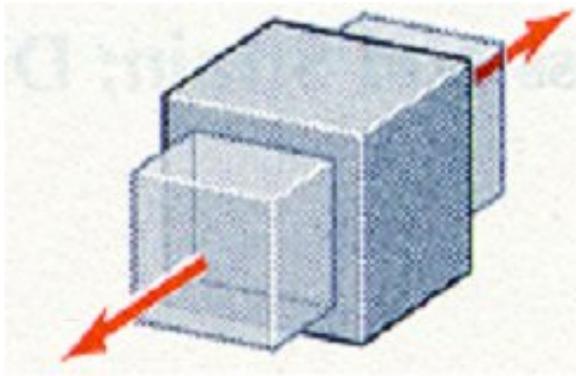
-Valores: ν Casi siempre está entre

(en mat. ing. Entre 0,25 y 0,35)

Aceros: $\nu = 0,33$

Aluminios: $\nu = 0,34$

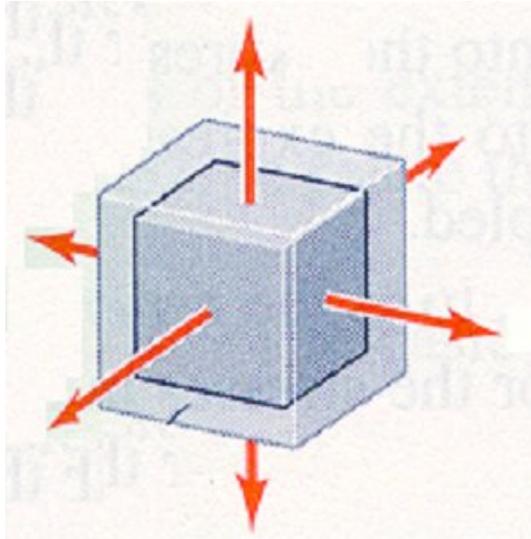
Polímeros: $\nu \approx 0,35$



$$\varepsilon_x = \frac{1}{E} \sigma_x$$

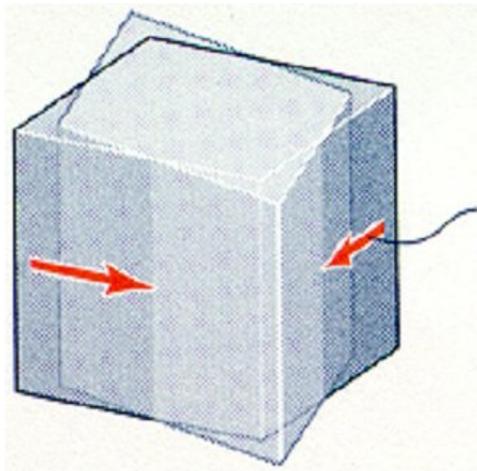
$$\varepsilon_y = -\frac{\nu}{E} \sigma_x$$

$$\varepsilon_z = -\frac{\nu}{E} \sigma_x$$

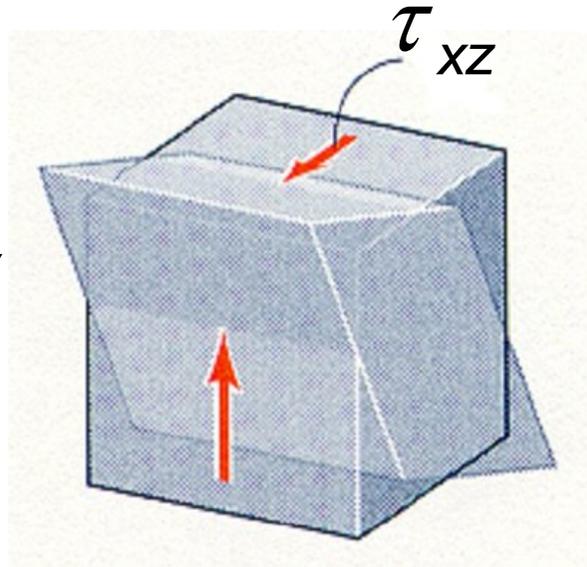


$$\left\{ \begin{array}{l} \varepsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)] \\ \varepsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x + \sigma_z)] \\ \varepsilon_z = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)] \end{array} \right.$$

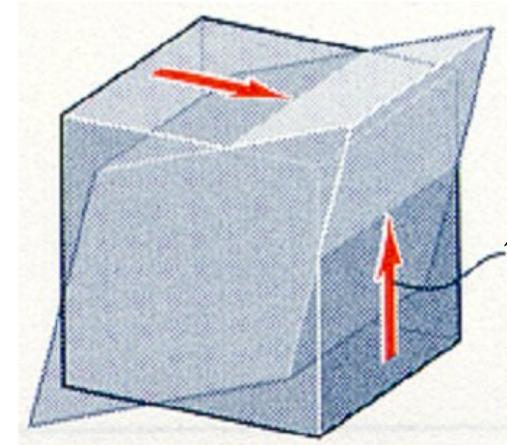
Leyes de Hooke (1ª parte)

 τ_{xy}

$$\tau_{xy} = G \cdot \gamma_{xy}$$

 τ_{xz}

$$\tau_{xz} = G \cdot \gamma_{xz}$$

 τ_{yz}

$$\tau_{yz} = G \cdot \gamma_{yz}$$

Leyes de Hooke (2ª parte)

$$G = \frac{E}{2 \cdot (1 + \nu)}$$

G: Módulo de cortadura
o de elasticidad transversal